Modular Symmetries of Threshold Corrections for Abelian Orbifolds with Discrete Wilson Lines

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Abstract

The modular symmetries of string loop threshold corrections for gauge coupling constants are studied in the presence of discrete Wilson lines for all examples of abelian orbifolds, where the point group is realised by the action of Coxeter elements or generalised Coxeter elements on the root lattices of the Lie groups.

1 Introduction

Orbifold compactifications of string theory [1, 2] possess various moduli, which are background fields corresponding to marginal deformations of the corresponding conformal field theory, including radii and angles of the underlying six dimensional torus. The spectrum of states for an orbifold is invariant under certain discrete transformations of the moduli, together with the winding numbers and momenta, referred to as modular symmetries [3, 4, 5, 6, 7, 8, 9, 10. These modular symmetries also appear as symmetries of the string loop threshold corrections [11, 12, 13, 14, 15, 16] which are important for the unification of gauge coupling constants. In this case, it is only the transformations of the moduli associated with fixed planes of twisted sectors of the orbifold theory that are relevant, and it is these particular modular symmetries we shall focus on here. Moreover, the form of the threshold corrections, which is constrained by the modular symmetries, determines the form of the non-perturbative superpotential due to gaugino condensation in the hidden sector and the effective potential, the minimization of which determines the values of the T and U moduli [17, 18, 19, 20, 21, 22, 23].

In the absence of Wilson lines, provided all twisted sector fixed planes are such that the six-torus T^6 can be decomposed as the direct sum $T^2 \oplus T^4$ with the fixed plane lying in T^2 , the group of modular symmetries of the threshold corrections is a product of $\mathrm{PSL}(2,\mathbb{Z})$ factors, one for each of the T and U moduli associated with the fixed planes. When such a decomposition is not possible (the non- $T^2 \oplus T^4$ case) the group of modular symmetries is in general a product of congruence subgroups [24, 25, 26] of $\mathrm{PSL}(2,\mathbb{Z})$. Wilson lines can also break the $\mathrm{PSL}(2,\mathbb{Z})$ modular symmetries [27, 28, 29] or further break [30] the congruence subgroups of $\mathrm{PSL}(2,\mathbb{Z})$.

It is our purpose here to classify all possible modular symmetry groups associated with threshold corrections for abelian $(Z_N \text{ and } Z_N \otimes Z_M)$ Coxeter and generalised Coxeter orbifolds, for abitrary choices of (discrete) Wilson lines. In section 2, the Coxeter and generalised Coxeter abelian orbifolds are classified. In section 3, the modular symmetry groups in the presence of Wilson lines are derived in the $T^2 \oplus T^4$ cases, in the sense discussed above, and in section 4 they are derived for the non- $T^2 \oplus T^4$ cases. Section 5 contains our conclusions.

2 Coxeter and Generalised Coxeter Orbifolds

A large class of abelian $(Z_N \text{ and } Z_N \otimes Z_M)$ orbifolds, the Coxeter orbifolds, can be obtained by taking the underlying lattice of the six-torus to be a

direct sum of Lie group root lattices and constructing the generators of the point group from Coxeter elements, generalised Coxeter elements or their powers for the various root lattices. A Coxeter element is the product of all the Weyl reflections of the root lattice. When the Dynkin diagram possesses an outer automorphism, we can also make a generalised Coxeter element by using those Weyl reflections associated with points in the Dynkin diagram that are not permuted by the outer automorphism together with one of the permuted Weyl reflections and the outer automorphism itself [31].

The only abelian groups that are able to act as automorphisms of a 6 dimensional lattice and produce exactly N=1 supersymmetry in the four dimensional compactified theory [1] are Z_N and $Z_M \otimes Z_N$ discrete subgroups of SU(3). These groups are given in tables 1 and 2 together with the action of the point group on the 3 complex planes in the space basis (i.e. with the bosonic degrees of freedom for the string on the compact manifold $X^1 \dots X^6$, written as the combinations $\frac{1}{\sqrt{2}}(X^1+iX^2)$, $\frac{1}{\sqrt{2}}(X^3+iX^4)$, and $\frac{1}{\sqrt{2}}(X^5+iX^6)$.) We need all possible choices of Lie group root lattices and Coxeter or generalised Coxeter elements which are able to realise these point groups. The order N of the Coxeter element is given by [31],

$$N = \frac{\text{number of non - zero roots}}{\text{rank of Lie algebra}} \tag{1}$$

In the case of a generalised Coxeter element, the rank of the algebra is replaced by an effective rank which is the rank reduced by the order of the outer automorphism minus one. The possible root lattices of dimensions less than or equal to 6 where the Coxeters or generalised Coxeters realise the various relevant Z_N point groups are given in table 3.

Even if the correct Z_N point group is realised by Coxeters or generalised Coxeters acting on Lie group root lattices, it is still necessary to check that their eigenvalues correspond to the correct action of the point group element on the complex planes in the space basis. This eliminates many possibilities. All possible choices of lattices for Coxeter and generalised Coxeter Z_N orbifolds have already been presented in [31], and are included in table 1 for convenience. For $Z_N \times Z_M$ orbifolds, some examples have already been given [32, 33]. If we insist on realising the point group using only Coxeters and generalised Coxeters but not their powers, the only possibilities are as in table 2. Some $Z_N \times Z_M$ point groups cannot be realised at all in this way. Appendix B contains the explicit action of the point group on the lattices for each Z_N or $Z_M \times Z_N$ example. The matrices for the various Coxeter and generalised Coxeter elements involved are given in appendix A.

In the absence of Wilson lines, the modular symmetries of threshold corrections and the threshold corrections themselves have already been calculated

for all Z_N Coxeter orbifolds [24, 25, 26] with non-decomposable twisted sector fixed planes. It remains to carry out the calculations for the generalised Coxeter orbifold Z_6 -II-f with a non- $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector. This is done in appendix C. None of the $Z_M \times Z_N$ example have non- $T_2 \oplus T_4$ planes.

3 Effect of Wilson Lines on Modular Symmetries for Decomposable Fixed Planes

As discussed in the introduction, it is the orbifold twisted sectors that possess fixed planes that are relevant to threshold corrections to gauge coupling constants. In this section, we shall discuss the modular symmetries associated with these twisted sectors in the presence of Wilson lines for the simplest case where the 6 torus T^6 can be decomposed as a direct sum $T^2 \oplus T^4$ with the fixed plane lying in the T^2 .

The case of Z_N Coxeter or generalised Coxeter orbifolds is discussed first. Let the Wilson line associated with the lattice vector e_a^i be denoted by A_a^I where **I** is a space index for the $E_8 \times E_8$ degrees of freedom and **a** is a lattice index for T^6 . The possible values for the Wilson lines are constrained by the usual [35] homomorphism and worldsheet modular invariance conditions. For a Z_N orbifold these are given by,

$$NA_a^I \in \Lambda_{E_8 \times E_8} \tag{2}$$

where $\Lambda_{E_8 \times E_8}$ is the $E_8 \times E_8$ lattice, and

$$N(\sum_{I} (nV^{I} + r_{a}A_{a}^{I})^{2} - n^{2}v^{2}) = 0 \pmod{2}$$
(3)

where n = 0, 1 ... N - 1, $r_a = 0, 1, ... N - 1$, V^I is the embedding of the point group element θ in $E_8 \times E_8$ and the action of θ in the *j*th complex plane is $e^{2\pi i v_j}$, j = 1, 2, 3.

$$N\sum_{I} (A_a^I)^2 = 0 \pmod{2} \tag{4}$$

$$N\sum_{I}A_{a}^{I}A_{b}^{I}=0\pmod{1}, a\neq b \tag{5}$$

$$N\sum_{I}V^{I}A_{a}^{I}=0\pmod{1}. \tag{6}$$

If the action of the point group element θ on the basis vectors of the compact manifold is

$$\theta: e_a \to \Theta_{ab}e_b$$
 (7)

then

$$A_a = \Theta_{ab}A_b + \Lambda_{E_8 \times E_8} \tag{8}$$

Identifies equivalent Wilson lines and contains the homomorphism condition (2). Equivalent Wilson lines are listed in appendix B for the various orbifolds. Moreover, by subtracting off appropriate lattice vectors we can choose lattice vectors in the region

$$\sum_{I=1}^{9} (A_a^I)^2 \le 1, \ \sum_{I=9}^{16} (A_a^I)^2 \le 1 \tag{9}$$

where the two conditions are seen to apply to the components of the Wilson line in the first and second E_8 factors of the gauge group separately. For the purpose of defining modular symmetries it is more convenient to work in terms of the matrix A_{Ab} defined by

$$A_{aB}^{T} = \sum_{I} A_a^{I} E_B^{I} \tag{10}$$

where E_A^I is a basis for the $E_8 \times E_8$ lattice. We can write (10) as

$$A_{aB}^{T} = A_{a}^{I} X_{IB}^{-1} \tag{11}$$

where X is the matrix

$$X = \frac{1}{2} \begin{pmatrix} 2 & -2 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 2 & -2 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 2 & -2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 2 & -2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 2 & -2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 2 & 2 \\ -1 & -1 & -1 & -1 & -1 & 1 & 1 & -1 \end{pmatrix}$$
 (12)

In this formulation [27, 28, 36] acceptable Wilson lines must satisfy

$$A(I-Q) \in Z \tag{13}$$

and

$$\frac{1}{2}A^{T}CA(I-Q) + \frac{1}{2}(I-Q^{*})A^{T}CA \in Z$$
(14)

where

$$Q = \Theta^T \tag{15}$$

and

$$Q^* \equiv (Q^{-1})^T \tag{16}$$

These conditions reflect the fact that the action of the point group must be an automorphism of the whole Narain lattice in the presence of Wilson lines [36]. Equations (13),(14) and (8) are slightly more restrictive than (4),(5) and (8), and in practice, we find it convenient to generate Wilson lines consistent with (4),(5) and (8) and then retain only those which also satisfy (13) and (14). For a specific choice of embedding of the point group we would also have to satisfy (6).

In the case of a $T^2 \oplus T^4$ fixed plane, the problem of determining the modular symmetries for the moduli associated with this plane reduces to a 2 dimensional problem [29]. If T and, in the case of a Z_2 plane, U, are the moduli associated with this fixed plane, then the full PSL(2,Z) group of modular transformations may be written as

$$T \to \frac{aT+b}{cT+d}, \ a, b, c, d \in \mathbb{Z}, \ ad-bc=1$$
 (17)

and

$$U \to \frac{a'U + b'}{c'U + d'}, \ a', b', c', d' \in Z, \ a'd' - b'c' = 1$$
 (18)

If the fixed plane is a Z_k fixed plane with $k \neq 2$ i.e. if the action of the point group in that complex plane is Z_k with $k \neq 2$, then only the T modulus occurs as a variable parameter of the orbifold model.

In general, the Wilson lines associated with this plane break the PSL(2,Z) modular groups to subgroups. For the T modular transformations, the conditions that determine this subgroup are [29]

$$cA \in Z$$
 (19)

$$\frac{c}{2}A^TCA \in Z \tag{20}$$

$$cAJA^TC \in Z \tag{21}$$

$$cAJA^{T}C \in Z$$

$$(1-d)A - \frac{c}{2}AJA^{T}CA \in Z$$

$$(21)$$

$$(1-a)CA - \frac{c}{2}CAJA^{T}CA \in Z \tag{23}$$

$$(1 - \frac{a}{2} - \frac{d}{2})A^TCA - \frac{c}{4}A^TCAJA^TCA \in Z$$
 (24)

where C is the Cartan metric for $E_8 \times E_8$ and

$$J = \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix}. \tag{25}$$

For the U modular transformations, the conditions that determine the unbroken subgroup are

$$A(I - F^{-1}) \in Z \tag{26}$$

$$A^{T}CA - \frac{1}{2}A^{T}CAF^{-1} - \frac{1}{2}F^{T}A^{T}CA \in Z$$
 (27)

where

$$F = \begin{pmatrix} d' & b' \\ c' & a' \end{pmatrix} \tag{28}$$

In (19)–(27) the fixed plane has been treated as an independent 2 dimensional plane and A and A^T have been truncated to the relevant two columns and rows respectively, which correspond to the fixed plane.

We have determined all possible modular symmetry groups in the presence of Wilson lines for the $T_2 \oplus T_4$ fixed planes of Z_N Coxeter and generalised Coxeter orbifolds. These are given in appendix D along with examples of Wilson lines that break the full $PSL(2,\mathbb{Z})$ group to these subgroups. For the case of a $T_2 \oplus T_4$ plane the resulting modular groups do not depend directly on the specific Z_N orbifold, but only on the action of the point group in that fixed plane. However, if there are Wilson lines present in other complex planes they can affect the allowed values of the Wilson lines in the fixed plane through the world sheet modular invariance conditions or (14), because the Cartan matrix C links rows of A^T corresponding to different complex planes. In that case, the full action of the point group is of importance because of its influence on inequivalent Wilson lines in the other complex planes. We have presented all modular groups permitted for the fixed plane with nonzero Wilson lines only in the fixed plane. With non-zero Wilson lines also present in other complex planes the possibilities are reduced because of the restriction of the choices of Wilson lines in the fixed plane just discussed. Specific choices of the point group embedding will further limit the choices of Wilson lines and so the possible modular groups.

For the $Z_M \times Z_N$ orbifolds, the allowed Wilson lines are determined by equivalence conditions associated with both point group elemnents θ and ω (as listed in appendix B) and by the worldsheet modular invariance conditions [35] defined for the $\theta^k \omega^l$ twisted sector

$$N'\left(\sum_{I} (kA^{I} + lB^{I} + r_{a}A_{a}^{I})^{2} - (ka + lb)^{2}\right) = 0 \pmod{2}$$
 (29)

where k = 0, 1, ..., M - 1, l = 0, 1, ..., N - 1, N' is the order of $\theta^k \omega^l$, A^I and B^I are the embeddings of θ and ω in the $E_8 \times E_8$ and the action of θ

and ω on the *j*th complex plane is $e^{2\pi i a_j}$, j=1,2,3, and $e^{2\pi i b_i}$, i=1,2,3. The integers r_a take values $0,1,\ldots,N'-1$.

In general, there could be two sets of conditions of the type (13) and (14) to satisfy, one for $Q(\theta)$ and one for $Q(\omega)$. However, by inspection of appendix B we see that for the most part, only one of $Q(\theta) = \Theta^T Q(\omega) = \Omega^T$ acts non–trivially in a particular fixed plane, or $Q(\theta)$ and $Q(\omega)$ both act in the same way. The only cases where $Q(\theta)$ and $Q(\omega)$ act differently are when one acts as $C^T(SU(3))$ and the other acts as $C^T(SU(3)^{[2]})$. However, in these cases there is no breaking of the PSL(2,Z) modular groups. The resulting modular symmetry groups in the presence of Wilson lines in the fixed plane are given in appendix E.

4 Effect of Wilson Lines on Modular Symmetries for non- $T_2 \oplus T_4$ Fixed Planes

When a fixed plane in an orbifold twisted sector is such that the 6 torus T^6 can not be decomposed into a direct sum $T^2 \oplus T^4$ with the fixed plane lying in the T^2 , the associated modular symmetry groups for T and U moduli are, in general, already broken to subgroups of PSL(2,Z) even in the absence of Wilson lines [24, 25, 26]. In the presence of Wilson lines further breaking of the symmetry can occur. A systematic method of calculating the resulting modular symmetry groups has been given elsewhere [30]. The system of equations that determine these modular groups depends on two matrices [38], which we call R and K. The role of these two matrices is that of allowing the initially 6 dimensional problem to be reduced to a 2 dimensional form. In appendix E we list all the R and K matrices for the models considered and in appendix F we explain the derivation of these matrices and thus how they relate to the notation in previous papers ([30] and [33]). There are no $Z_M \times Z_N$ orbifolds with point groups elements realised by Coxeter or generalised Coxeter elements with non- $T_2 \oplus T_4$ fixed planes, with the exeception of $Z_2 \times Z_2$ which was considered in [37].

To solve for the modular symmetries, it is convenient to construct an 8×2 matrix, which we write simply as A_T in the following, which contains the relevant Wilson line components involved in the problem and is obtained in the reduction from the 6 dimensional problem, as detailed in appendix F. The modular symmetries, then, are given by the constraint equations, which are for the T modulus

$$cA_TRJK \in Z$$
 (30)

$$cA_TRJKA_T^tC \in Z$$
 (31)

$$(1-d)A_TR - \frac{1}{2}cA_TRJKA_T^tCA_TR \in Z \quad (32)$$

$$cKA_T^tC \in Z$$
 (33)

$$\frac{1}{2}cKA_T^tCA_TR \in Z \quad (34)$$

$$\frac{1}{2}cA_T^tCA_TRJK \in Z \quad (35)$$

$$(1 - a - \frac{1}{2}cA_T^tCARJK)A_T^tC \in Z \quad (36)$$

$$(1 - \frac{1}{2}a - \frac{1}{2}d)A_T^t C A_T R - \frac{1}{4}cA_T^t C A_T R J K A_T^t C A_T R + bK^{-1}J \in Z$$
 (37)

(38)

and for the U modulus

$$A_T R(I - M) \in Z \tag{39}$$

$$K^{-1}M^*K \in Z \tag{40}$$

$$A_T^t C A_T R - \frac{1}{2} A_T^t C A_T R M - \frac{1}{2} K^{-1} M^* K A_T^t C A_T R \in Z$$
 (41)

where J is given by (25)

$$M = \begin{pmatrix} a' & -b' \\ -c' & d' \end{pmatrix} = F^{-1} \tag{42}$$

and M^* is defined to be $(M^{-1})^t$. The integer coefficients a, b, c, d and a', b', c', d' in the constraint equations are the coefficients of the modular transformations (17,18) on the T and U moduli respectively.

5 Conclusions

The moduli dependent corrections to gauge coupling constants in orbifold compactifactions are a possible mechanism for reconciling the unification scale for the standard model gauge coupling constants with string theory. We have carried out a systematic study of the possible modular symmetry groups in the presence of quantised Wilson lines for all Coxeter orbifolds. Modular symmetry constrains the functional form that moduli dependent threshold corrections can take and, in some cases, this constraint is strong enough to explicitly determine the threshold correction. The results of the present paper are a first step in that direction for all Coxeter orbifolds. The modular symmetry groups obtained are in some cases congruence subgroups and in other cases more exotic subgroups of PSL(2,Z).

Appendices

A Coxeter and Generalised Coxeter Elements

For each Lie group root lattice the action of the Coxeter element or generalised Coxeter element on the basis vectors e_a of the root lattice is given below. The action of the Weyl reflection σ_a associated with the basis vector e_a on the basis vector e_b is defined to be

$$\sigma_a(e_b) = e_b - \frac{2e_a \cdot e_b}{e_a \cdot e_a} e_a \tag{43}$$

The generalised Coxeter elements also contain cyclic permutations of the basis vectors

A.1 SU(2)

Dynkin diagram \bigcirc Coxeter $\theta = \sigma_1$ $\theta e_1 = -e_1$

A.2 SU(3)

Dynkin diagram \bigcirc Coxeter $\theta = \sigma_1 \sigma_2$ $\theta e_1 = e_2, \ \theta e_2 = -e_1 - e_2$ Eigenvalues $exp(\pm 2\pi i/3)$ Generalised Coxeter $\theta = \sigma_2 \begin{pmatrix} 1 & 2 \\ 2 & 1 \end{pmatrix}$ $\theta e_1 = -e_2, \ \theta e_2 = e_1 + e_2$ Eigenvalues $exp(\pm 2\pi i/6)$

$A.3 \quad SU(4)$

Dynkin diagram 0—0—0Coxeter $\theta = \sigma_1 \sigma_2 \sigma_3$ $\theta e_1 = e_2, \ \theta e_2 = e_3, \ \theta e_3 = -e_1 - e_2 - e_3$ Eigenvalues $-1, \pm i$ Generalised Coxeter $\theta = \sigma_1 \sigma_2 \begin{pmatrix} 1 & 3 \\ 3 & 1 \end{pmatrix}$

Orbifold	θ	Lattice
Z_3	(1,1,-2)/3	$SU(3) \times SU(3) \times SU(3)$
$Z_4 - a$	(1,1,-2)/4	$SU(4) \times SU(4)$
$Z_4 - b$	(1,1,-2)/4	$SU(4) \times SO(5) \times SU(2)$
Z_4-c	(1,1,-2)/4	$SO(5) \times SU(2) \times SO(5) \times SU(2)$
$Z_6 - I - a$	(-2,1,1)/6	$SU(3) \times G_2 \times G_2$
$Z_6 - I - b$	(-2,1,1)/6	$SU(3) \times SU(3)^{[2]} \times SU(3)^{[2]}$
$Z_6 - I - c$	(-2,1,1)/6	$SU(3) \times SU(3)^{[2]} \times G_2$
$Z_6 - II - a$	(2,1,-3)/6	$SU(6) \times SU(2)$
$Z_6 - II - b$	(2,1,-3)/6	$SU(3) \times SO(8)$
$Z_6 - II - c$	(2,1,-3)/6	$SU(3) \times SO(7) \times SU(2)$
$Z_6 - II - d$	(2,1,-3)/6	$SU(3) \times G_2 \times SO(4)$
$Z_6 - II - e$	(2,1,-3)/6	$SU(3) \times SU(3)^{[2]} \times SO(4)$
$Z_6 - II - f$	(2,1,-3)/6	$SU(3) \times SU(4)^{[2]} \times SU(2)$
$Z_6 - II - g$	(2,1,-3)/6	$SU(3) \times Sp(6) \times SU(2)$
Z_7	(1,2,-3)/7	SU(7)
$Z_8 - I - a$	(1, -3, 2)/8	$SO(9) \times SO(5)$
$Z_8 - I - b$	(1, -3, 2)/8	$SO(8)^{[2]} \times SO(5)$
$Z_8 - II - a$	(1,3,-4)/8	$SO(10) \times SU(2)$
$Z_8 - II - b$	(1,3,-4)/8	$SO(9) \times SO(4)$
$Z_8 - II - c$	(1,3,-4)/8	$SO(8)^{[2]} \times SO(4)$
$Z_{12}-I-a$	(1, -5, 4)/12	E_6
$Z_{12} - I - b$	(1, -5, 4)/12	$F_4 \times SU(3)$
$Z_{12} - I - c$	(1, -5, 4)/12	$SO(8)^{[3]} \times SU(3)$
$Z_{12} - II - a$	(1,5,-6)/12	$F_4 \times SO(4)$
$Z_{12}-II-b$	(1,5,-6)/12	$SO(8)^{[3]} \times SO(4)$

Table 1: Coxeter and generalised Coxeter Z_N orbifolds. For the point group generator θ we display (v_1, v_2, v_3) such that the action of θ in the complex orthogonal basis is $(e^{2\pi i v_1}, e^{2\pi i v_2}, e^{2\pi i v_2})$. When the generalised Coxeter element with outer automorphism of order p acts on the root lattice is written as $G^{[p]}$.

Orbifold	θ	ω	Lattice
$Z_2 \times Z_2$	(1,0,-1)/2	(0,1,-1)/2	$(SO(4))^3$
$Z_3 \times Z_3$	(1,0,-1)/3	(0,1,-1)/3	$(SU(3))^3$
$Z_2 \times Z_4$	(1,0,-1)/2	(0,1,-1)/4	
$Z_4 \times Z_4$	(1,0,-1)/4	(0,1,-1)/4	$(SO(5))^3$
$Z_2 \times Z_6$	(1,0,-1)/2	(0,1,-1)/6	—
$Z_2 \times Z_6'$	(1,0,-1)/2	(0,1,-1)/6	
$Z_3 \times Z_6 - a$	(1,0,-1)/3	(0,1,-1)/6	$(SU(3))^3$
$Z_3 \times Z_6 - b$	(1,0,-1)/3	(0,1,-1)/6	$SU(3) \times G_2 \times SU(3)$
$Z_6 \times Z_6 - a$	(1,0,-1)/6	(0,1,-1)/6	$(G_2)^3$
$Z_6 \times Z_6 - b$	(1,0,-1)/6	(0,1,-1)/6	$(G_2)^2 \times SU(3)$
$Z_6 \times Z_6 - c$	(1,0,-1)/6	(0,1,-1)/6	$G_2 \times (SU(3))^2$
$Z_6 \times Z_6 - d$	(1,0,-1)/6	(0,1,-1)/6	$(SU(3))^3$

Table 2: Coxeter and generalised Coxeter $Z_M \times Z_N$ orbifolds. For the point group generator θ we display (v_1, v_2, v_3) such that the action of θ in the complex orthogonal basis is $(e^{2\pi i v_1}, e^{2\pi i v_2}, e^{2\pi i v_2})$ and similarly for ω .

Point Group	Possible Root Lattices
Z_2	SU(2), SO(4)
Z_3	SU(3)
Z_4	SU(4), SO(5)
Z_6	SU(6), SO(8), SO(7), Sp(6),
	$G_2, SU(3)^{[2]}, SU(4)^{[2]}$
Z_7	SU(7)
Z_8	$SO(10), SO(9), Sp(8), SO(8)^{[2]}$
Z_{12}	$SO(13), Sp(12), F_4, E_6, SO(8)^{[3]}$

Table 3: Root lattices of dimension ≤ 6 where the Coxeter or generalised Coxeter element generate Z_N point groups. The generalised Coxeter elements with outer automorphism of order p acint on the root lattice is written as $G^{[p]}$.

 $\theta e_1 = e_1 + e_2 + e_3, \ \theta e_2 = -e_1 - e_2, \ \theta e_3 = e_2$ Eigenvalues $-1, exp(\pm 2\pi i/6)$

A.4 SU(6) 1 2 3 Dynkin diagram \bigcirc \bigcirc \bigcirc

Coxeter $\theta = \sigma_1 \sigma_2 \sigma_3 \sigma_4 \sigma_5$

 $\theta e_1 = e_2, \ \theta e_2 = e_3, \ \theta e_3 = e_4, \ \theta e_4 = e_5, \ \theta e_5 = -e_1 - e_2 - e_3 - e_4 - e_5$ Eigenvalues $-1, exp(\pm 2\pi i/3), exp(\pm 2\pi i/6)$

$A.5 \quad SU(7)$

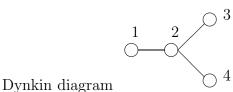
$A.6 \quad SO(5)$

Dynkin diagram

Coxeter $\theta = \sigma_1 \sigma_2$ $\theta e_1 = e_1 + 2e_2, \ \theta e_2 = -e_1 - e_2$ Eigenvalues $\pm i$

$A.7 \quad SO(7)$

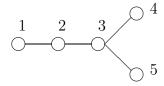
A.8 SO(8)



Coxeter $\theta = \sigma_1 \sigma_2 \sigma_3 \sigma_4$ $\theta e_1 = e_2, \ \theta e_2 = e_1 + e_2 + e_3 + e_4, \ \theta e_3 = -e_1 - e_2 - e_3, \ \theta e_4 = -e_1 - e_2 - e_4$ Eigenvalues $-1 \ (twice), \ exp(\pm 2\pi i/6)$ First generalised Coxeter $\theta = \sigma_1 \sigma_2 \sigma_3 \begin{pmatrix} 3 & 4 \\ 4 & 3 \end{pmatrix}$ $\theta e_1 = e_2, \ \theta e_2 = e_3, \ \theta e_3 = e_1 + e_2 + e_4, \ \theta e_4 = -e_1 - e_2 - e_3,$ Eigenvalues $exp(\pm 2\pi i/8), exp(\pm 10\pi i/8)$ Second generalised Coxeter $\theta = \sigma_1 \sigma_2 \begin{pmatrix} 1 & 3 & 4 \\ 3 & 4 & 1 \end{pmatrix}$ $\theta e_1 = e_1 + e_2 + e_3, \ \theta e_2 = -e_1 - e_2, \ \theta e_3 = e_1 + e_2 + e_4, \ \theta e_4 = e_2$ Eigenvalues $exp(\pm 2\pi i/12), exp(\pm 7\pi i/6)$

A.9 SO(9)

A.10 SO(10)



Dynkin diagram

Coxeter $\theta = \sigma_1 \sigma_2 \sigma_3 \sigma_4 \sigma_5$

 $\theta e_1 = e_2, \ \theta e_2 = e_3, \ \theta e_3 = e_1 + e_2 + e_3 + e_4 + e_5, \ \theta e_4 = -e_1 - e_2 - e_3 - e_4, \ \theta e_5 = -e_1 - e_2 - e_3 - e_5$

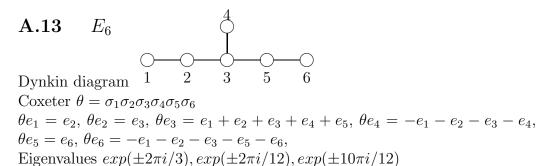
Eigenvalues -1, $exp(\pm 2\pi i/8)$, $exp(\pm 6\pi i/8)$

A.11 G_2 Dynkin diagram Coxeter $\theta = \sigma_1 \sigma_2$ $\theta e_1 = e_1 + 2e_2, \ \theta e_2 = -e_1 - e_2$ Eigenvalues $\pm i$

A.12
$$F_4$$
 1 2 3 Dynkin diagram \bigcirc

Coxeter
$$\theta = \sigma_1 \sigma_2 \sigma_3 \sigma_4$$

 $\theta e_1 = e_2, \ \theta e_2 = e_1 + e_2 + e_3, \ \theta e_3 = e_4, \ \theta e_4 = -2e_1 - 2e_2 - e_3 - e_4$
Eigenvalues $exp(\pm 2\pi i/12), exp(\pm 10\pi i/12)$



$A.14 \operatorname{Sp}(6)$

Dynkin diagram 0 0 0 Coxeter $\theta = \sigma_1 \sigma_2 \sigma_3$ $\theta e_1 = e_2, \ \theta e_2 = e_1 + e_2 + e_3, \ \theta e_3 = -2e_1 - 2e_2 - e_3$ Eigenvalues $-1, exp(\pm 2\pi i/6)$

$A.15 \quad Sp(8)$

B Coxeter and Generalised Coxeter Orbifolds

For each orbifold, the action of the point group on the complex space basis $exp(2\pi i[v_1,v_2,v_3])$ is specified by (v_1,v_2,v_3) . The action of the point group on the lattice basis is given in terms of Coxeter elements or generalised Coxeter elements for the root lattices involved, with the Coxeter element for the root lattice of the Lie group G written as C(G) and any generalised Coxeter element written as $C(G^{[p]})$ where p is the order of the outer automorphism involved. Then the action in the lattice basis of the point group element θ is given in terms of a matrix Θ composed of Coxeter element matrices, such that the effect of θ on the basis vectors e_a of the lattice is $e_a \to \Theta_{ab}e_b$. The order of the point group for the various $T_2 \oplus T_4$ and non- $T_2 \oplus T_4$ twested

sector fixed planes (in the sense of the introduction) is given. Finally, the equivalent Wilson line A_i corresponds to the basis vector e_i .

B.1
$$Z_3$$
 $\theta = (1, 1, -2)/3$ $(SU(3))^3$

 $\Theta = [C(SU(3)), C(SU(3)), C(SU(3))]$ no fixed planes.

 $A_2 \approx A_1, A_4 \approx A_3, A_6 \approx A_5, 3A_1 \approx 3A_2 \approx 3A_5 \approx 0$

B.2
$$Z_4 - a$$
 $\theta = (1, 1, -2)/4$ $(SU(4))^2$

 $\Theta = [C(SU(4)),\ C(SU(4))]$

 $non-T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_3 \approx A_2 \approx A_1, A_6 \approx A_5 \approx A_4, 4A_1 \approx 4A_4 \approx 0$

B.3
$$Z_4 - b$$
 $\theta = (1, 1, -2)/4$ $SU(4) \times SO(5) \times SU(2)$

 $\Theta = [C(SU(4)), \ C(SO(5)), \ C(SU(2))]$

 $non-T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_3 \approx A_2 \approx A_1, \ 4A_1 \approx A_4 \approx 2A_5 \approx 2A_6 \approx 0$

B.4
$$Z_4-c$$
 $\theta = (1,1,-2)/4$ $SO(5) \times SU(2) \times SO(5) \times SU(2)$

 $\Theta = [C(SO(5)), C(SU(2)), C(SO(5)), C(SU(2))]$

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_1 \approx A_4 \approx 2A_2 \approx 2A_3 \approx 2A_5 \approx 2A_6 \approx 0$

B.5
$$Z_6 - I - a$$
 $\theta = (-2, 1, 1)/6$ $SU(3) \times G_2 \times G_2$

 $\Theta = [C(SU(3)), \ C(G_2), \ C(G_2)]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $A_2 \approx A_1, \, 3A_1 \approx A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.6
$$Z_6 - I - b$$
 $\theta = (-2, 1, 1)/6$ $SU(3) \times SU(3)^{[2]} \times SU(3)^{[2]}$

 $\Theta = [C(SU(3)), C(SU(3)^{[2]}), C(SU(3)^{[2]})]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $A_2 \approx A_1, \ 3A_1 \approx A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.7
$$Z_6 - I - c$$
 $\theta = (-2, 1, 1)/6$ $SU(3) \times SU(3)^{[2]} \times G_2$

 $\Theta = [C(SU(3)), C(SU(3)^{[2]}), C(G_2)]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $A_2 \approx A_1$, $3A_1 \approx A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.8
$$Z_6 - II - a$$
 $\theta = (2, 1, -3)/6$ $SU(6) \times SU(2)$

 $\Theta = [C(SU(6)), C(SU(2))]$

 $non-T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $non-T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $6A_1 \approx 2A_6 \approx 0, A_5 \approx A_4 \approx A_3 \approx A_2 \approx A_1$

B.9
$$Z_6 - II - b$$
 $\theta = (2, 1, -3)/6$ $SU(3) \times SO(8)$

 $\Theta = [C(SU(3)), C(SO(8))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $non-T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_2 \approx A_1, \ 3A_1 \approx 0, \ A_3 \approx A_4, \ 2A_3 \approx 2A_5 \approx 2A_6 \approx 0, \ A_3 \approx -A_5 - A_6$

B.10
$$Z_6 - II - c$$
 $\theta = (2, 1, -3)/6$ $SU(3) \times SO(7) \times SU(2)$

 $\Theta = [C(SU(3)), \ C(SO(7)), \ C(SU(2))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $non-T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_2 \approx A_1, \, 3A_1 \approx A_3 \approx A_4 \approx 2A_5 \approx 2A_6 \approx 0$

B.11
$$Z_6 - II - d$$
 $\theta = (2, 1, -3)/6$ $SU(3) \times G_2 \times SO(4)$

 $\Theta = [C(SU(3)), C(G_2), C(SO(4))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_2 \approx A_1, \, 3A_1 \approx A_3 \approx A_4 \approx 2A_5 \approx 2A_6 \approx 0$

B.12
$$Z_6 - II - e \quad \theta = (2, 1, -3)/6 \quad SU(3) \times SU(3)^{[2]} \times SO(4)$$

 $\Theta = [C(SU(3)), C(SU(3)^{[2]}), C(SO(4))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_2 \approx A_1, \, 3A_1 \approx A_3 \approx A_4 \approx 2A_5 \approx 2A_6 \approx 0$

B.13
$$Z_6 - II - f$$
 $\theta = (2, 1, -3)/6$ $SU(3) \times SU(4)^{[2]} \times SU(2)$

 $\Theta = [C(SU(3)), C(SU(4)^{[2]}), C(SU(2))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_2 \approx A_1, \ 3A_1 \approx A_3 \approx 0, \ A_4 \approx A_5, \ 2A_4 \approx 2A_6 \approx 0$

B.14
$$Z_6 - II - g$$
 $\theta = (2, 1, -3)/6$ $SU(3) \times Sp(6) \times SU(2)$

 $\Theta = [C(SU(3)), C(Sp(6)), C(SU(2))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $non-T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_2 \approx A_1, \ 3A_1 \approx 2A_3 \approx 0, \ A_4 \approx A_5, \ 2A_4 \approx 2A_6 \approx 0$

B.15
$$Z_7$$
 $\theta = (1, 2, -3)/7$ $SU(7)$

 $\Theta = [C(SU(7))]$

no fixed planes

 $A_6 \approx A_5 \approx A_4 \approx A_3 \approx A_2 \approx A_1, \ 7A_1 \approx 0$

B.16
$$Z_8 - I - a$$
 $\theta = (1, -3, 2)/8$ $SO(9) \times SO(5)$

 $\Theta = [C(SO(9)), \ C(SO(5))]$

 $T_2 \oplus T_4$ Z_4 fixed plane in the θ^4 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx A_5 \approx 2A_4 \approx 2A_6 \approx 0$

B.17
$$Z_8 - I - b$$
 $\theta = (1, -3, 2)/8$ $SO(8)^{[2]} \times SO(5)$

 $\Theta = [C(SO(8)^{[2]}), C(SO(5))]$

 $T_2 \oplus T_4$ Z_4 fixed plane in the θ^4 twisted sector.

 $A_4 \approx A_3 \approx A_2 \approx A_1, \ 2A_1 \approx A_5 \approx 2A_6 \approx 0$

B.18
$$Z_8 - II - a$$
 $\theta = (1, 3, -4)/8$ $SO(10) \times SU(2)$

 $\Theta = [C(SO(10)), \ C(SU(2))]$

 $non-T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_1 \approx A_2 \approx A_3, \ A_4 \approx -A_5, \ 2A_4 \approx A_3, \ 2A_3 \approx 2A_6 \approx 0$

B.19
$$Z_8 - II - b$$
 $\theta = (1, 3, -4)/8$ $SO(9) \times SO(4)$

 $\Theta = [C(SO(9)), C(SO(4))]$

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx 2A_4 \approx 2A_5 \approx 2A_6 \approx 0$

B.20
$$Z_8 - II - c$$
 $\theta = (1, 3, -4)/8$ $SO(8)^{[2]} \times SO(4)$

 $\Theta = [C(SO(8)^{[2]}), C(SO(4))]$

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx A_4$, $2A_1 \approx 2A_5 \approx 2A_6 \approx 0$

B.21
$$Z_{12} - I - a$$
 $\theta = (1, -5, 4)/12$ E_6

 $\Theta = [C(E_6)]$

 $non-T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx A_5, \ 3A_5 \approx A_6 \approx 0$

B.22
$$Z_{12} - I - b$$
 $\theta = (1, -5, 4)/12$ $F_4 \times SU(3)$

 $\Theta = [C(F_4), C(SU(3))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx 0, \ A_5 \approx A_6, \ 3A_6 \approx 0$

B.23
$$Z_{12} - I - c$$
 $\theta = (1, -5, 4)/12$ $SO(8)^{[3]} \times SU(3)$

 $\Theta = [C(SO(8)^{[3]}), C(SU(3))]$

 $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx 0, \ A_5 \approx A_6, \ 3A_6 \approx 0$

B.24
$$Z_{12} - II - a$$
 $\theta = (1, 5, -6)/12$ $F_4 \times SO(4)$

 $\Theta = [C(F_4), C(SO(4))]$

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx 0, \ 2A_5 \approx 2A_6$

B.25
$$Z_{12} - II - b$$
 $\theta = (1, 5, -6)/12$ $SO(8)^{[3]} \times SO(4)$

 $\Theta = [C(SO(8)^{[3]}), C(SO(4))]$

 $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx 0, \ 2A_5 \approx 2A_6$

B.26
$$Z_2 \times Z_2$$
 $\theta = (1, 0, -1)/2$ $\omega = (0, 1, -1)/2$ $(SO(4))^3$

 $\Theta = [C(SO(4)), I, C(SO(4))] \quad \Omega = [I, C(SO(4)), C(SO(4))]$

 $T_2 \oplus T_4$ (I, Z_2) , (Z_2, I) and (Z_2, Z_2) fixed planes in the θ , ω and $\theta\omega$ twisted sectors respectively.

 $2A_1 \approx 2A_2 \approx 2A_3 \approx 2A_4 \approx 2A_5 \approx 2A_6 \approx 0$

B.27
$$Z_3 \times Z_3$$
 $\theta = (1, 0, -1)/3$ $\omega = (0, 1, -1)/3$ $(SU(3))^3$

 $\Theta = [C(SU(3)), I, C(SU(3))] \quad \Omega = [I, C(SU(3)), C(SU(3))]$

 $T_2 \oplus T_4$ (I, Z_3) , (Z_3, I) and (Z_3, Z_3) fixed planes in the θ^k , ω^k and $(\theta \omega^2)^k$ twisted sectors respectively.

 $A_1 \approx A_2, A_3 \approx A_4, A_5 \approx A_6, 3A_1 \approx 3A_3 \approx 3A_5 \approx 0$

B.28
$$Z_4 \times Z_4$$
 $\theta = (1, 0, -1)/4$ $\omega = (0, 1, -1)/4$ $(SO(5))^3$

 $\Theta = [C(SO(5)), I, C(SO(5))] \quad \Omega = [I, C(SO(5)), C(SO(5))]$

 $T_2 \oplus T_4$ (I, Z_4) , (Z_4, I) and (Z_4, Z_4) fixed planes in the θ^k , ω^k and $(\theta^2 \omega^2)^k$ twisted sectors respectively.

 $A_1 \approx A_3 \approx A_5 \approx 0, \ 2A_2 \approx 2A_4 \approx 2A_6 \approx 0$

B.29
$$Z_3 \times Z_6 - a$$
 $\theta = (1, 0, -1)/3$ $\omega = (0, 1, -1)/6$ $(SU(3))^3$

 $\Theta = [C(SU(3)), I, C(SU(3))] \quad \Omega = [I, C(SU(3)^{[2]}), C(SU(3)^{[2]})]$

 $T_2 \oplus T_4$ (I, Z_6) , (Z_3, I) and (Z_3, Z_6) fixed planes in the θ^k , ω^k and $(\theta \omega^4)^k$ twisted sectors respectively.

 $A_1 \approx A_2$, $3A_1 \approx 0$, $A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.30
$$Z_3 \times Z_6 - b$$
 $\theta = (1, 0, -1)/3$ $\omega = (0, 1, -1)/6$ $SU(3) \times G_2 \times SU(3)$

 $\Theta = [C(SU(3)), I, C(SU(3))] \quad \Omega = [I, C(G_2), C(SU(3)^{[2]})]$

 $T_2 \oplus T_4$ (I, Z_6) , (Z_3, I) and (Z_3, Z_6) fixed planes in the θ^k , ω^k and $(\theta \omega^4)^k$ twisted sectors respectively.

 $A_1 \approx A_2, \ 3A_1 \approx 0, \ A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.31
$$Z_6 \times Z_6 - a$$
 $\theta = (1, 0, -1)/6$ $\omega = (0, 1, -1)/6$ $(G_2)^3$

 $\Theta = [C(G_2), I, C(G_2)] \ \Omega = [I, C(G_2), C(G_2)]$

 $T_2 \oplus T_4(I, Z_6)$, (Z_6, I) and (Z_6, Z_6) fixed planes in the θ^k , ω^k and $(\theta \omega^5)^k$ twisted sectors respectively.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.32
$$Z_6 \times Z_6 - b$$
 $\theta = (1, 0, -1)/6$ $\omega = (0, 1, -1)/6$ $(G_2)^2 \times SU(3)$

 $\Theta = [C(G_2), \ I, \ C(SU(3)^{[2]})] \ \Omega = [I, \ C(G_2), \ C(SU(3)^{[2]})] \ T_2 \oplus T_4 \ (I, Z_6), \ (Z_6, I) \ and \ (Z_6, Z_6) \ fixed \ planes \ in \ the \ \theta^k, \ \omega^k \ and \ (\theta\omega^5)^k \ twisted \ sectors \ respectively.$

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.33
$$Z_6 \times Z_6 - c$$
 $\theta = (1, 0, -1)/6$ $\omega = (0, 1, -1)/6$ $G_2 \times (SU(3))^2$

 $\Theta = [C(G_2), \ I, \ C(SU(3)^{[2]})] \ \Omega = [I, \ C(SU(3)^{[2]}), \ C(SU(3)^{[2]})]$ $T_2 \oplus T_4 \ (I, Z_6), \ (Z_6, I) \ and \ (Z_6, Z_6) \ fixed \ planes \ in \ the \ \theta^k, \ \omega^k \ and \ (\theta\omega^5)^k$ twisted sectors respectively.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

B.34
$$Z_6 \times Z_6 - d$$
 $\theta = (1, 0, -1)/6$ $\omega = (0, 1, -1)/6$ $(SU(3))^3$

 $\Theta = [C(SU(3)^{[2]}), \ I, \ C(SU(3)^{[2]})] \ \Omega = [I, \ C(SU(3)^{[2]}), \ C(SU(3)^{[2]})]$ $T_2 \oplus T_4(I, Z_6), \ (Z_6, I) \ and \ (Z_6, Z_6) \ fixed \ planes \ in \ the \ \theta^k, \ \omega^k \ and \ (\theta\omega^5)^k$ twisted sectors respectively.

 $A_1 \approx A_2 \approx A_3 \approx A_4 \approx A_5 \approx A_6 \approx 0$

C Modular Symmetries of New Orbifolds

We now present the calculation of the modular symmetries and threshold corrections for $Z_6 - II - f$ without Wilson lines. The derivation uses the methods applied earlier [24, 25, 26] to Coxeter Z_N orbifolds. The matrix Q representing the action of the point group is Θ^T where

$$\Theta = (C(SU(4)^{[2]}), C(SU(3)), C(SU(2))) \tag{44}$$

as in appendix B. There is a non– $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector. Solving

$$Q^2w = w (45)$$

and

$$(Q^*)^2 p = p \tag{46}$$

where

$$Q^* \equiv (Q^T)^{-1} \tag{47}$$

gives the solutions W_{soln} and p_{soln} for the winding numbers and momenta in the θ^2 twisted sector

$$w_{soln} = \begin{pmatrix} n_1 \\ 2n_1 \\ -n_1 \\ 0 \\ 0 \\ n_6 \end{pmatrix} \tag{48}$$

and

$$p_{soln} = \begin{pmatrix} 0 \\ m_2 \\ -m_2 \\ 0 \\ 0 \\ m_6 \end{pmatrix} \tag{49}$$

by The world sheet momentum P is given by

$$P = p_{soln}^T w_{soln} = m_{\perp}^T K^T n_{\perp} \tag{50}$$

where

$$m_{\perp} = \begin{pmatrix} m_2 \\ m_6 \end{pmatrix} , \ n_{\perp} = \begin{pmatrix} n_1 \\ n_6 \end{pmatrix} \tag{51}$$

Thus,

$$K = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix} \tag{52}$$

This matrix K has the same form as for the θ^2 twisted sector of the Z_6 –II–c orbifold [25, 26] despite the very different form of the w_{soln} and p_{soln} . Thus the modular symmetry group associated with the Z_2 fixed planes is $\Gamma^0(3)_T \times \Gamma_0(3)_U$ in the notation of earlier work [24, 25, 26] for congruence subgroups of PSL(2,Z), where the first factor refers to the T modulus and the second factor to the U modulus.

In addition, because we are dealing with the same orbifold appart from the lattice, the fundamental sectors and the construction of the renormalisation

group co–efficient $b_a^{N=2}$ from the co–efficients $b_a^{(I,\theta^2)}, b_a^{(\theta^4,\theta^2)}, b_a^{(\theta^4,\theta^4)}$ and $b_a^{(\theta^2,I)}$ for the various twisted sectors is the same as for Z_6 -II-c. With K as above, the matrix A involved in the construction of the partition function is

$$A = \begin{pmatrix} n_1 & l_1/3 \\ n_2 & l_2 \end{pmatrix} \tag{53}$$

just as for Z_6 -II-c, and we obtain for the contribution of these sectors to the threshold correction

$$\Delta_a = -2b_a^{(I,\theta^2)} ln(kT_2|\eta(T)|^4 U_2|\eta(U)|^4) - 2b_a^{(I,\theta^2)} ln(kT_2|\eta(T/3)|^4 U_2|\eta(3U)|^4) (54)$$

Modular Subgroups for $T_2 \oplus T_4$ Orbifolds D

We now list all the obtainable modular symmetries for $Z_2, Z, 3$ and Z_4 planes, where the plane lies completely in the T^2 sublattice, for all choices of Wilson lines consistent with modular and point group invariance. For each modular group we also provide an example Wilson line which yields this symmetry.

Z_2 Plane D.1

For the T modulus there are 7 possible modular groups:

1. PSL(2,Z)

$$A = \mathbf{0}$$

2.
$$a, d = 1 \mod 4, c = 0 \mod 4$$
 and $a, d = 3 \mod 4, c = 0 \mod 4$

8 mod 16 and $a, d = 3 \mod 4$, $c = 0 \mod 16$ and $a = 3 \mod 4$, $d = 1 \mod 4$, $c = 8 \mod 16$

```
1. PSL(2,Z)
A = \mathbf{0}
5. a, d = 1 \mod 4, b, c = 0 \mod 4 and a, d = 1 \mod 4, b, c = 2 \mod 4 and
a, d = 3 \mod 4, b, c = 0 \mod 4 and a, d = 3 \mod 4, b, c = 2 \mod 4
0 \mod 4, c = 0 \mod 2
0 \mod 2, c = 0 \mod 4
```

D.2 Z_3 Plane

The U modulus is fixed for a Z_3 plane. For the T modulus there are 2 modular groups:

1.
$$PSL(2,Z)$$

$$A = \mathbf{0}$$

2.
$$a, d = 1 \mod 3, c = 0 \mod 3$$

D.3 Z_4 Plane

The U modulus is fixed for a Z_4 plane. For the T modulus there are 2 modular groups:

1.
$$PSL(2,Z)$$

$$A = \mathbf{0}$$

2.
$$\Gamma_0(2)$$

Modular Subgroups for non- $T_2 \oplus T_4$ Orb- \mathbf{E} ifolds

We now list all the obtainable modular symmetries of fixed planes, where the orbifold cannot be decomposed as $T_2 \oplus T_4$ for all choices of Wilson lines consistent with modular and point group invariance. For each modular group we also provide an example Wilson line which yields this symmetry.

E.1 Z_4 -**a** $(SU(4)^2)$

There is a non– $T_2\oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector. $R=\begin{pmatrix}2&0\\0&2\end{pmatrix}$ $K=\begin{pmatrix}2&0\\0&2\end{pmatrix}$

$$R = \begin{pmatrix} 2 & 0 \\ 0 & 2 \end{pmatrix} \quad K = \begin{pmatrix} 2 & 0 \\ 0 & 2 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A =

For the T modulus there are 6 modular groups:

1.
$$\Gamma^{0}(2)$$

$$A = \mathbf{0}$$

2. $a = 1 \mod 4$, $b, c = 0 \mod 2$, $d = 1 \mod 2$

```
For the U modulus there are 9 modular groups:
1. PSL(2,Z)
A = \mathbf{0}
2. a, d = 1 \mod 2, c = 0 \mod 2
0 \mod 4, d = 1 \mod 4 and a = 1 \mod 4, b = 0 \mod 4, c = 2 \mod 4, d = 0 \mod 4
```

E.2 Z_4 -**b** $SU(4) \times SO(5) \times SU(2)$

There is a non– $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

$$R = \begin{pmatrix} 2 & 0 \\ 0 & 1 \end{pmatrix} \quad K = \begin{pmatrix} 2 & 0 \\ 0 & 1 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: $A = \begin{pmatrix} A_1 \\ A_6 \end{pmatrix}$

For the T modulus there are 9 modular groups:

1. $\Gamma^{0}(2)$

$$A = \mathbf{0}$$

2. $a, d = 1 \mod 4, b = 0 \mod 2, c = 0 \mod 4 \text{ and } a, d = 3 \mod 4, b = 0$ $0 \mod 2, c = 0 \mod 4$

 $b=0\bmod 2,\,c=2\bmod 4,\,d=1\bmod 2$

 $0 \mod 2, c = 0 \mod 8 \text{ and } a, d = 1 \mod 4, b = 1 \mod 2, c = 4 \mod 8 \text{ and } a, d = 1 \mod 8$

Z_6 -II-a $SU(6) \times SU(2)$ E.3

There is a non- $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector and a non- $T_2 \oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector. $R = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix}$ $K = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix}$

$$R = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix} \quad K = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A = $\begin{pmatrix} A_1 \\ A_6 \end{pmatrix}$

The θ^2 sector:

For the T modulus there are 6 modular groups:

1. $\Gamma^{0}(3)$

```
A = \mathbf{0}
2. a, d = 1 \mod 4, b = 0 \mod 3, c = 0 \mod 4 \text{ and } a, d = 3 \mod 4, b = 0
0 \mod 3, c = 0 \mod 4
5. a = 1 \mod 12, b = 0 \mod 3, c = 0 \mod 8, d = 1 \mod 4 and a = 7 \mod 12,
b = 0 \mod 3, c = 0 \mod 8, d = 3 \mod 4
For the U modulus there are 7 modular groups:
1. \Gamma_0(3)
A = \mathbf{0}
5. a = 1 \mod 4, b = 0 \mod 2, c = 0 \mod 12, d = 1 \mod 12 and a = 3 \mod 4,
b = 1 \mod 2, c = 3 \mod 6, d = 4 \mod 6
 The \theta^3 sector:

R = \begin{pmatrix} 2 & 0 \\ 0 & 2 \end{pmatrix} K = \begin{pmatrix} 2 & 0 \\ 0 & 2 \end{pmatrix}
```

Wilson lines as stated here correspond to the six component line as: A =

For the T modulus there are 3 modular groups:

1. $\Gamma^{0}(2)$

$$A = \mathbf{0}$$

2.
$$a = 1 \mod 6$$
, $b = 0 \mod 2$, $c = 0 \mod 3$, $d = 1 \mod 3$
$$A = \frac{1}{6} \begin{pmatrix} 2 & 1 & 1 & 0 & 0 & 0 & 0 & 2 & 1 & 1 & 0 & 0 & 0 & 0 \\ 2 & 1 & 1 & 0 & 0 & 0 & 0 & 2 & 1 & 1 & 0 & 0 & 0 & 0 \end{pmatrix}$$
3. $a, d = 1 \mod 3$, $b = 0 \mod 2$, $c = 0 \mod 3$

Z_6 -II-b $SU(3) \times SO(8)$ E.4

There is a non–
$$T_2 \oplus T_4$$
 Z_2 fixed plane in the θ^2 twisted sector.
$$R = \begin{pmatrix} 0 & -1 \\ -1 & 0 \end{pmatrix} \quad K = \begin{pmatrix} 2 & 1 \\ 1 & 2 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A =

For the T modulus there are 4 modular groups:

1. $\Gamma^{0}(3)$

$$A = \mathbf{0}$$

For the U modulus there are 4 modular groups:

1.
$$\frac{1}{3}a + \frac{2}{3}b - \frac{2}{3}c - \frac{1}{3}d \in \mathbb{Z}$$
, $\frac{2}{3}a + \frac{1}{3}b - \frac{1}{3}c - \frac{2}{3}d \in \mathbb{Z}$
 $A = \mathbf{0}$

3.
$$\frac{1}{3}a + \frac{2}{3}b - \frac{2}{3}c - \frac{1}{3}d \in \mathbb{Z}$$
, $\frac{2}{3}a + \frac{1}{3}b - \frac{1}{3}c - \frac{2}{3}d \in \mathbb{Z}$, $a = 1 \mod 2$, $b = 0 \mod 2$, $d = 1 \mod 2$, $c = 0 \mod 2$, $-\frac{1}{2} - \frac{1}{3}a - \frac{5}{12}b + \frac{11}{12}c + \frac{5}{6}d \in \mathbb{Z}$, $-\frac{1}{2} - \frac{1}{4}a - \frac{1}{2}b + \frac{1}{2}c + \frac{3}{4}d \in \mathbb{Z}$,

Z_6 -II-c $SU(3) \times SO(7) \times SU(2)$

There is a non– $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

$$R = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \quad K = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A = $\begin{pmatrix} A_5 \\ A_6 \end{pmatrix}$

For the T modulus there are 5 modular groups:

1. $\Gamma^{0}(3)$

 $A = \mathbf{0}$

2. $a = 1 \mod 4$, $b = 0 \mod 3$, $c = 0 \mod 4$, $d = 1 \mod 4$ and $a = 3 \mod 4$, $b = 0 \mod 3, c = 0 \mod 4, d = 3 \mod 4$

For the U modulus there are 7 modular groups:

1. $\Gamma_0(3)$

 $A = \mathbf{0}$

3.
$$a, d = 1 \mod 2, c = 0 \mod 6$$

 $0 \mod 2$, $c = 0 \mod 6$

Z_6 -II-f $SU(3) \times SU(4)^{[2]} \times SU(2)$

There is a non– $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

$$R = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \quad K = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A =

For the T modulus there are 2 modular groups:

1. $\Gamma^{0}(3)$

$$A = \mathbf{0}$$

For the U modulus there are 4 modular groups:

1. $\Gamma_0(3)$

$$A = \mathbf{0}$$

2. $a, d = 1 \mod 2, c = 0 \mod 6$

Z_6 -II-g $SU(3) \times Sp(6) \times SU(2)$

There is a non- $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector.

$$R = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} \quad K = \begin{pmatrix} 3 & 0 \\ 0 & 1 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A = $\begin{pmatrix} A_5 \\ A_6 \end{pmatrix}$

For the T modulus there are 2 modular groups:

1. $\Gamma^{0}(3)$

 $A = \mathbf{0}$

2. $a, d = 1 \mod 2, b = 0 \mod 3, c = 0 \mod$

1. $\Gamma_0(3)$

 $A = \mathbf{0}$

2. $a, d = 1 \mod 2, c = 0 \mod 6$

Z_8 -II-a $SO(10) \times SU(2)$ E.8

There is a non– $T_2 \oplus T_4$ Z_2 fixed plane in the θ^2 twisted sector. $R = \begin{pmatrix} 2 & 0 \\ 0 & 1 \end{pmatrix}$ $K = \begin{pmatrix} 2 & 0 \\ 0 & 1 \end{pmatrix}$

$$R = \begin{pmatrix} 2 & 0 \\ 0 & 1 \end{pmatrix} \quad K = \begin{pmatrix} 2 & 0 \\ 0 & 1 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A = $\begin{pmatrix} A_4 \\ A_6 \end{pmatrix}$

For the T modulus there are 6 modular groups:

1. $\Gamma^{0}(2)$

 $A = \mathbf{0}$

2. $a, d = 1 \mod 4$, $b = 0 \mod 2$, $c = 0 \mod 4$ and $a, d = 3 \mod 4$, b = 0 $0 \mod 2, c = 0 \mod 4$

```
6. a = 1 \mod 4, b = 0 \mod 2, c = 0 \mod 4, d = 1 \mod 2
For the U modulus there are 6 modular groups:
1. \Gamma_0(2)
A = \mathbf{0}
2. a, d = 1 \mod 4, c = 0 \mod 8 and a, d = 3 \mod 4, c = 0 \mod 8
```

Z_{12} -I-a E_6 $\mathbf{E.9}$

There is a non– $T_2\oplus T_4$ Z_3 fixed plane in the θ^3 twisted sector. $R=\begin{pmatrix}2&0\\0&2\end{pmatrix}$ $K=\begin{pmatrix}2&0\\0&2\end{pmatrix}$

$$R = \begin{pmatrix} 2 & 0 \\ 0 & 2 \end{pmatrix} \quad K = \begin{pmatrix} 2 & 0 \\ 0 & 2 \end{pmatrix}$$

Wilson lines as stated here correspond to the six component line as: A = $\begin{pmatrix} A_1 \\ A_4 \end{pmatrix}$

For the T modulus there are 2 modular groups:

1. $\Gamma^{0}(2)$

$$A = \mathbf{0}$$

F Calculation of R and K matrices

The matrices R and K allow the constraints on the modular symmetry group of non- $T_2 \oplus T_4$ orbifolds to be expressed in a 2-dimensional form. The constraints are obtained by ensuring that the physical winding and momentum states in the fixed plane transform properly under the modular transformations. The physical winding numbers and momenta in the plane must be expressable in terms of only two independent components in each case. In particular we wish to express the contribution to the worldsheet momentum P in terms of the two independent values of the momenta and windings, hence K is defined by

$$P = p_{soln}^T w_{soln} = m_{\perp}^T K^T n_{\perp} \tag{55}$$

where p_{soln} and w_{soln} are the solutions to $(Q^*)^k p = p$ and $Q^k w = w$ respectively and are six dimensional vectors and m_{\perp}, n_{\perp} are the corresponding two dimensional momentum and winding numbers. An example of the calculation of K for a specific orbifold was given in appendix C. Similarly, the R matrix is introduced when expressing the constraints in the presence of non-zero Wilson lines in terms of only two independent lines. The Wilson lines involved in the problem are those which correspond to the windings of w_{soln} . For example, in the case of the Z_6 -II-f of appendix C, w_{soln} is given by $w_{soln} = (n_1, 2n_1, -n_1, 0, 0, n_6)^T$, and so the Wilson lines involved in the problem are the components A_1 , A_2 , A_3 associated with windings in one direction in the fixed plane and A_6 associated with the windings in the other direction. It might appear that there are then in fact 4 different Wilson line components involved in the problem, but the number of independent Wilson line components is reduced to only two in all problems by the point group invariance condition, which in this case yields the relations $A_2 \approx A_3$, $A_1 \approx 2A_2 \approx 0$. So in the case of the Z_6 -II-f orbifold the Wilson line contribution can be expressed in terms of the independent components A_2 and A_6 . The R matrix is then defined by

$$Aw_{soln} = A_{\perp}Rn_{\perp} \tag{56}$$

where A is the six dimensional Wilson line and A_{\perp} is the two dimensional line consisting of the two independent components of the six dimensional line which contribute, as discussed above, and n_{\perp} is as defined above.

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